

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization  
International Bureau



(43) International Publication Date  
11 April 2002 (11.04.2002)

PCT

(10) International Publication Number  
**WO 02/29487 A1**

(51) International Patent Classification<sup>7</sup>: **G02F 1/35**,  
G03H 1/26

Pottage, West Sussex RH10 5NY (GB). **BROTHER-  
TON-RATCLIFFE, David** [GB/GB]; Forest House,  
Parish Lane, Pease Pottage, West Sussex RH10 5NY (GB).

(21) International Application Number: PCT/GB01/04460

(74) Agents: **JEFFREY, Philip, Michael** et al.; Frank B. Dehn  
& Co., 179 Queen Victoria Street, London EC4V 4EL  
(GB).

(22) International Filing Date: 8 October 2001 (08.10.2001)

(25) Filing Language: English

(81) Designated States (*national*): AE, AG, AI, AM, AT, AT  
(utility model), AU, AZ, BA, BB, BG, BR, BY, BZ, CA,  
CH, CN, CO, CR, CU, CZ, CZ (utility model), DE, DE  
(utility model), DK, DK (utility model), DM, DZ, EC, EE,  
EE (utility model), ES, FI, FI (utility model), GB, GD, GE,  
GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ,  
LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN,  
MW, MX, MZ, NO, NZ, PH, PL, PT, RO, RU, SD, SE, SG,  
SI, SK, SK (utility model), SL, TJ, TM, TR, TT, TZ, UA,  
UG, US, UZ, VN, YU, ZA, ZW.

(26) Publication Language: English

(30) Priority Data:  
0024533.2 6 October 2000 (06.10.2000) GB

(71) Applicant (*for all designated States except US*): **GEOLA  
TECHNOLOGIES LTD.** [GB/GB]; Forest House, Parish  
Lane, Pease Pottage, West Sussex RH10 5NY (GB).

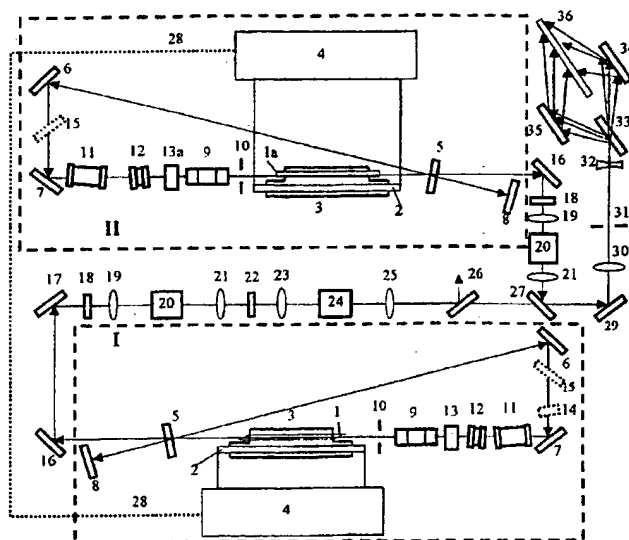
(72) Inventors; and

(75) Inventors/Applicants (*for US only*): **RODIN, Alexey**  
[LT/LT]; Pylimo 11-8, Vilnius, 2001 (LT). **VERGNES,**  
**Florian** [FR/GB]; Forest House, Parish Lane, Pease

(84) Designated States (*regional*): ARIPO patent (GH, GM,  
KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZW), Eurasian  
patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European  
patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE,  
IT, LU, MC, NL, PT, SE, TR), OAPI patent (BF, BJ, CF,

[Continued on next page]

(54) Title: PULSED MULTIPLE COLOUR LASER SYSTEM



(57) Abstract: A pulsed multiple colour laser system is disclosed having particular application for incorporation into a digital holographic printer for producing RGB colour reflection holograms. A Nd:YLF crystal (1) in a laser cavity is excited to produce an emission at 1313 nm which is frequency converted by doubling to 656.3 nm and by tripling to 437.7 nm. In a separate cavity a similar Nd:YLF crystal (1a) is synchronously or asynchronously excited to produce an emission at 1047.1 nm (or at the related line of 1053 nm) which is frequency converted by doubling to 523.6 nm (or 526.5 nm). The emissions at 437.7 nm and 656.5 nm are combined co-linearly with the emission at 523.6 nm (or 526.5 nm) to produce a single RGB pulsed laser beam.

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CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

*For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.*

**Published:**

— with international search report

## PULSED MULTIPLE COLOUR LASER SYSTEM

5       The present invention relates to a pulsed multiple colour laser system.

      Previous work on multiple colour pulsed lasers has been concentrated in two fields. The first is holographic interferometry and the second is military target designation. US-3818372 describes a pulsed Ruby  
10       laser that can be operated at two wavelengths and that has applications in holographic interferometry. This laser, however, is based on the principle of mechanically changing the rear mirror in order to produce different wavelength emissions. As a  
15       consequence, the time between the different wavelength emissions is large.

      US-6078606 describes a general method for obtaining multiple colour laser pulse emissions at controllable interpulse separations that may reach zero. The class  
20       of lasers described herein has particular applications in military target designation but may also be useful in holographic interferometry. These lasers are based on the design of a single active laser crystal and multiple cavities. Population inversion depletion by a single  
25       wavelength of this active medium is avoided by the stress birefringence effect that also orthogonally polarizes the chromatic emissions in a two-wavelength system.

      In the field of holographic printing the lasers which  
30       have been employed to date are all continuous wave (CW) lasers. However, severe problems exist concerning the use of CW lasers in such an application due to the inherent sensitivity of the holographic writing process to vibration. The use of CW lasers in commercial  
35       holography printing machines therefore results in severe operational problems which limits the operational speed and choice of location.

Holographic printers can be designed to produce several forms of holograms. Some of these forms only require a monochromatic laser. Other forms such as the full-colour reflection hologram require a multiple  
5 colour laser for realistic commercial implementation. Until now no commercial holographic printers printing full-colour reflection holograms have appeared on the market. However, some considerable work has been done  
10 in the laboratory fabrication of such holograms using CW lasers.

Full-colour reflection holograms are of particular commercial interest. Typically, three component laser emissions are required in a suitable laser corresponding to a red, blue and green signal. The wavelengths of  
15 these three primary laser sources must satisfy three conditions. They must firstly fall inside an optimum area of the standard chromaticity chart. Secondly, they must fall inside the same wavelength zone as standard commercial lighting sources and thirdly they must fall  
20 inside the area of acceptable human eye sensitivity. Pulsed lasers useful for RGB holography must preferably have Gaussian or quasi-Gaussian beam profiles, plane polarized emissions and a reasonably large temporal coherence length (ranging from 1 mm to 10 m). Different  
25 applications warrant various energies, repetition rates and pulse to pulse reproducibilities.

Various CW lasers exist today on an off-the-shelf basis that satisfy these requirements. This is not the case for pulsed lasers.

30 According to a first aspect of the present invention there is provided a pulsed multiple colour laser system as claimed in claim 1.

Further aspects of the present invention are recited by the further independent claims.

35 In contrast to the prior art, according to the preferred embodiment the various chromatic emissions are able to be synchronous. This is not possible using

mechanical manipulation of component optical parts as in US-3818372.

Preferably, the chromatic laser emissions fall inside an optimum area of the standard chromaticity chart so that such emissions can be used to produce a wide range of visually perceived colours by selective combination. Further preferably, each chromatic emission falls inside the same wavelength zone occupied by standard commercial lighting sources and that of an acceptable human eye sensitivity. This is not possible with the laser system disclosed in US-6078606 for instance.

A yet further preferred feature of the present invention is that the relative energies and pulse lengths of each chromatic emission can be controlled independently and accurately. This is also in contrast to the system disclosed in US-6078606.

Advantageously, a preferred aspect of the present invention is that the laser system is capable of reliable single mode, single frequency generation. Accordingly, the pumping of each active medium responsible for a given wavelength emission can preferably be controlled. It is preferred that such pumping is low enough not to induce stress birefringence.

A further preferred feature of the present invention is that it does not use directly the fundamental emissions of the active laser elements, as in both of the examples of prior art given above, but rather uses their second and third harmonics.

According to the preferred embodiment, a Neodymium YLF crystal in a laser cavity is used to produce an emission at 1313 nm that is frequency converted by doubling to 656.5 nm and by tripling to 437.7 nm. In a separate cavity a similar Neodymium YLF crystal is excited to produce an emission at 1053 nm (or at the related line of 1047.1 nm) which is frequency converted by doubling to 526.5 nm (or 523.6 nm). The emissions at

437.7 nm, 526.5 nm and 656.5 nm are combined, preferably co-linearly (or in a less preferred embodiment non co-linearly) so as to produce a single RGB pulsed laser beam.

5        Various active and passive optical components in the laser are chosen so as to produce an optimum pulse energy ratio between the three wavelengths for a given application. Different designs may be used to attain a variety of pulse durations, energies and various beam  
10 parameters as described above and as required, for example, by different holographic printing applications.

      In another preferred embodiment the Nd:YLF crystals are replaced by Nd:YAP, Nd:YAG or Nd:BEL and the corresponding atomic transitions in these materials are  
15 utilized (Nd:YAG: 1064.2 nm giving 532.1 nm; 1318.8 nm giving 659.4 nm and 439.6 nm; 1338 nm giving 669 nm and 446 nm. Nd:YAP: 1064.3 nm or 1079.6 nm (preferred) or 1099 nm giving either 532.2 nm, 539.8 nm (preferred) or 549.5 nm; 1341.4 nm giving 670.7 nm and 447.1 nm.  
20 Nd:BEL: 1070 nm giving 535 nm; 1351 nm giving 675.5 nm and 450.3 nm).

      Other embodiments are also contemplated wherein any similar Nd atomic transitions in host matrices of other materials are utilized. As described above laser  
25 amplifiers may be used to amplify the fundamental radiation (corresponding to 1313 nm and 1053 nm (or 1047.1 nm) in Nd:YLF) before harmonic conversion and co-linear combination in order to achieve more energetic multiple colour emissions. The Nd:YLF transition line  
30 1321.2 nm may also be used to replace 1313 nm.

      Various embodiments of the present invention will now be described, by way of example only, and with reference to the accompanying drawings in which:

      Fig. 1 shows a conventional laser system comprising a  
35 single active laser crystal shared between two cavities producing emissions at two fundamental harmonics;

      Fig. 2 shows a passively Q-switched single stage

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single frequency multiple colour Nd:YLF/Nd:YAG laser according to a first embodiment of the present invention;

Fig. 3 shows a 2-stage multiple colour Nd:YLF/Nd:YAG laser according to a second embodiment of the present invention;

Fig. 4 shows an actively Q-switched single-stage single-frequency multiple colour Nd:YLF/Nd:YAG laser according to a third embodiment of the present invention;

Fig. 5 shows a 1-step or "Direct-Write" holographic printer; and

Fig. 6 shows an arrangement for producing a final white-light viewable hologram from a master or H1 hologram.

A conventional laser system is shown in Fig. 1. A laser medium 110, such as Nd:YAG, Nd:YLF or Ruby, is pumped by a flash lamp 112 which is driven by a laser excitation driver 114. Two partially overlapping laser cavities are defined by the optical paths 115, 116 and 117. The first of these cavities is defined by the optical path determined by the mirrors 120 and 124. The second cavity is determined by mirrors 120 and 126. These cavities partially overlap between the mirror 120 and the beam splitter 122.

Each of the two cavities is tuned to a different characteristic emission wavelength of the active element 110 (i.e.  $\lambda_1$  and  $\lambda_2$ ). The optical axis 115 defines the major axis of the system along which laser radiation travels. At one end of the optical axis 115 the mirror 120 is partially reflective at wavelengths  $\lambda_1$  and  $\lambda_2$ . The beam splitting device 122 is placed at a 45 degree angle and is coated to transmit light at  $\lambda_1$  and reflect light at  $\lambda_2$ . Initially the radiation emitted from the laser medium 110 contains both wavelengths. However, due to the length of the cavities and the coatings applied to mirrors 124 and 126 (mirror 124 is coated to

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be reflective at  $\lambda_1$  and mirror 126 is coated to be reflective at  $\lambda_2$ ) only light of one colour ends up propagating in a given cavity ( $\lambda_1$  along the optical path 116 and  $\lambda_2$  along the optical path 117).

5       The Q-switches 128 and 130 control the operation of the respective cavities. Laser excitation driver 114 drives a trigger generator 132 which activates the Q-switch 128. The output from the trigger generator 132 is applied to an adjustable delay unit 134 which retards  
10       the trigger pulse from the trigger generator 132 by an amount  $\Delta$ , this amount being controlled by the control unit 138.

      In operation the laser excitation driver initiates a lamp flash causing laser medium 110 to develop a  
15       population inversion. At the same time the trigger generator 132 triggers the Q-switch 128 causing a spike of radiation 140 at  $\lambda_1$  to propagate through elements 122, 128, 124, 128, 122, 110, 120 and out of the laser. After a predetermined time  $\Delta$  the trigger pulse from trigger  
20       generator 132 triggers the Q-switch 130 causing a second spike of radiation 142 at  $\lambda_2$  to propagate through elements 122, 130, 126, 130, 122, 110, 120 and out of the laser. In this way a 2-colour pulsed laser beam is produced.

25

Passively Q-switched Single-Stage Single Frequency  
Multiple colour Nd:YLF/Nd:YAG Laser

      Fig. 2 shows a first embodiment of the present  
30       invention. The laser system depicted is a multiple colour laser built around two Neodymium-doped Yttrium Lithium Fluoride (Nd:YLF) crystal ring oscillators I, II. Both oscillators are passively Q-switched and configured to generate TEM<sub>00</sub> single frequency radiation. Oscillator  
35       I is arranged to produce 1313 nm wavelength radiation and oscillator II is arranged to produce 1053 nm (or 1047 nm) wavelength radiation.



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The Nd:YLF crystal 1 (e.g. rod of 4x95 mm size AR-coated for 1313 and 1053 nm) in oscillator I is preferably provided with tilted edges (of about  $3^\circ$ ) to avoid parasitic excitation at 1053 nm. The Nd:YLF  
5 crystal 1a in oscillator II may however be provided with simply parallel edges. Both crystals are excited by a single linear xenon flashlamp 2 (typically of 5 mm bore diameter and 75 mm length) although other forms of pumping such as diodes could be used. Both pump  
10 chambers 3 have diffuse reflectors and liquid cooling circuits and are connected to synchronized laser power supplies 4.

The two ring laser cavities are very similar. Each consists of three ring cavity mirrors 5,6,7 comprising  
15 rear mirrors 6,7 and an output coupler 5. Typically, the reflectivity of the output coupler 5 is 80% in oscillator I and 45% in oscillator II. The optimal output coupler for the total 2 m cavity length was found to be meniscus with the radius of curvature of  $R = 15$  m.  
20 The return mirror 8 is used to suppress parasitic ring-cavity components although this could equally well be dealt with by any other non-reciprocal element such as an intracavity Faraday rotator coupled with a half waveplate or acousto-optic mirror. Element 9 is a Dove  
25 prism which improves the cavity stability against misalignment and also improves the beam structure by effecting a  $180^\circ$  field rotation at each pass through the cavity. An intracavity aperture 10 is used to suppress higher order transverse cavity modes. Two tilted Fabry-  
30 Perot etalons 11,12 act to suppress all but the required longitudinal cavity mode.

In oscillator I preferably a YAG:V<sup>3+</sup> passive Q-switch 13 is used (typically having initial transmission of  $T_0 = 55\%$ ) although alternatively a passive Q-switch based on  
35 polymers with polymethine dyes, Co<sup>2+</sup>:LMA, PbSe QD-doped phosphate glasses or an electro-optical Q-switch with feedback control could be used. In oscillator II a

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YAG:Cr passive Q-switch 13a is preferably used (typically having an initial transmission of  $T_0 = 35-50\%$ ) although alternatively a passive Q-switch based on GSGG:Cr, LiF crystals or an electro-optical Q-switch with feedback control could be used. Both oscillators I, II could be realized equally well with a 5-mirror ring scheme instead of the 3-mirror scheme as depicted in Fig. 2. In oscillator I such a 5-mirror scheme would improve suppression of parasitic radiation at 1053 nm.

10 Mirrors 16 direct the radiation produced by each laser oscillator towards wavelength conversion sections of the laser system.

The output of oscillator I is deflected by transfer mirror 17 and is then directed to half waveplate 18 which rotates the laser beam polarization by  $45^\circ$  and lens 19 which focuses the radiation into a second harmonic crystal 20 for efficient conversion to 656.5 nm. Preferably, the second harmonic crystal 20 is a II type AR-coated KTP crystal (5x5x12 mm) inside a temperature stabilized oven. Alternatively, the KTP crystal could be replaced by LBO, BBO or  $\text{LiNbO}_3$ .

20 The beam continues through collimating lens 21 restoring initial polarization of 1313 nm after half waveplate 22 for efficient non-linear mixing of the frequencies 1313 nm and 656.5 nm. The beam continues to the focusing lens 23 which is used to improve the efficiency of conversion at the non-linear crystal 24 to the third harmonic. Preferably, the third harmonic crystal 24 is a I-type LBO crystal (3x3x20 mm) inside a temperature stabilized oven. Alternatively, the LBO crystal could be replaced by BBO or DKDP. However, DKDP has a significantly lower conversion efficiency. Both fundamental, second and third harmonics continue to the collimating lens 25. The dielectric mirror 26 reflects the remaining fundamental radiation at 1313 nm allowing only the required radiation at 656.5 nm (typically of energy  $E = 3-4 \text{ mJ}$ , duration of  $\tau = 60-90 \text{ ns}$ ) and 437.7

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nm (typically of energy  $E = 2.8-3.5$  mJ, duration of  $\tau = 50-80$  ns) to continue.

The output of oscillator II follows a similar but simpler route through the half waveplate 18, focusing lens 19 and the KTP second harmonic crystal 20. Preferably, the second harmonic crystal 20 is a II-type KTP crystal (5x5x10 mm) inside a temperature stabilized oven. The second harmonic crystal 20 produces radiation at  $\bar{5}26.5$  (523.6) nm. Alternatively, the KTP crystal could be replaced by LBO, BBO, DKDP. However, the conversion efficiency in the case of DKDP will be sufficiently lower. The beam is then collimated by collimating lens 21.

Dielectric mirror 27 is arranged so as to reflect only the required radiation at 526.5 nm (typically of energy  $E = 4-8$  mJ, duration of  $\tau = 30-50$  ns) allowing the fundamental at 1053nm (or 1047.1 nm) to continue into a beam block (not shown).

Laser power supplies 4 are synchronized through cable 28 to ensure synchronously or asynchronously emission at 526.5 (523.6) nm, 437.7 nm and 656.5 nm wavelength.

The radiation emissions at 526.5 (523.6) nm, 437.7 nm and 656.5 nm are now co-linear. For purposes of illustration of use, the RGB laser beam is shown passing into a simplified holographic set-up comprising mirror 29, spatial beam filter formed by positive lens 30 and pinhole 31, negative lens 32, beam splitter 33, object beam and reference beam mirrors 34, 35 and holography plate 36.

Focusing and collimating lenses 19, 21, 23, 25 could be changed to beam diameter compressing telescopes if nonlinear frequency conversion crystals with rather critical angular phase-matching (e.g. DKDP, BBO) are used.

In an alternative embodiment the two Nd:YLF crystals 1, 1a could be replaced by non-birefringent Neodymium-doped Yttrium Aluminium Garnet (Nd:YAG) crystals.

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However, for stable laser operation two additional intracavity elements would then be required, namely a thin Fabry-Perot etalon 14 (e.g. a quartz etalon of 45  $\mu\text{m}$  thickness without dielectric coating) to suppress competitive generation of 1338 nm and a polarizer 15 to ensure the laser beams are linearly polarized at the output of oscillators I and II. In such a case oscillator I would be configured for 1064.2 nm wavelength generation and oscillator II would be configured for 1318.8 nm wavelength generation.

Nd:YAG is preferred for use as the active material for multi-colour laser operation at high-repetition rates ( $> 5\text{-}7\text{ Hz}$ ). This is because Nd:YAG is a higher gain material than Nd:YLF. As such, Nd:YAG requires less flashlamp pumping energy to attain the same population inversion. In addition Nd:YAG has a better thermal conductivity than Nd:YLF and so can conduct away heat faster and better than Nd:YLF, allowing it to tolerate more aggressive and faster pumping. However, Nd:YAG has a lower maximum stored energy than Nd:YLF and hence the output energy from the Nd:YAG oscillator is generally lower (for example at 659.4 nm typically  $E = 2.5\text{-}3\text{ mJ}$  and at 439.6 nm  $E = 2.0\text{ mJ}$ ). Also, Nd:YAG has a much bigger thermal lens than Nd:YLF and so care must be exercised to optimize the curvature of the output coupler 5 for a particular repetition rate when using Nd:YAG.

The duration of the various chromatic laser pulses may be extended to approximately 150 ns by varying the respective cavity length, the initial transmission coefficients of the passive Q-switches, and the output cavity mirror reflectivities. Further increase of the duration of the respective chromatic Q-switched pulses up to approximately 400 ns may be accomplished by the insertion of  $\text{ZnP}_2$  or  $\text{CdP}_2$  crystal plates into the respective cavities (based upon the operational principle of photodarkening).

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A free Running (no Q-switching) Single-Stage Multiple  
colour Nd:YLF/Nd:YAG Laser

5 The laser system according to the first embodiment  
may be converted into a free-running laser having output  
emissions in the microsecond regime (typically of  $\tau =$   
10-100  $\mu$ s pulse duration). This is useful in certain  
holographic applications. In order to convert the laser  
10 according to the first embodiment into such a free-  
running laser the Q-switches 13,13a may be removed and  
the lenses 19,21,23,25 changed to provide a higher  
energy density on each of the non-linear crystals thus  
assuring an adequate harmonic conversion efficiency.

15 Two stage Single Frequency Single Mode Multiple colour  
Nd:YLF/Nd:YAG laser

Fig. 3 shows a schematic diagram of a second  
embodiment of the present invention. The laser depicted  
20 is a multiple colour laser system built around two  
Neodymium-doped Yttrium Lithium Fluoride (Nd:YLF)  
crystal ring oscillators and two Neodymium-doped Yttrium  
Lithium Fluoride (Nd:YLF) amplifiers. The oscillators  
I,II are identical to those described in relation to the  
25 first embodiment. Hence, as before, Oscillator I is  
configured for 1313 nm generation and oscillator II is  
configured for 1053 nm (or 1047.1 nm) generation.

The output of each oscillator I,II is directed into a  
telescope 16 in order to match each pump beam to the  
30 cross-sectional size of the amplifier. The two two-pass  
amplifiers 17,18,19,20,21,22,23 are schematically  
identical although the individual optical components are  
designed for operation at different wavelengths. Each  
amplifier comprises a thin film dielectric polarizer 17,  
35 a Faraday Rotator 18, a 45° polarization rotator 19, an  
amplifier pump chamber with Nd:YLF laser rod, a linear  
Xenon flashlamp and diffuse reflector 20, an amplifier

power supply 21, a focusing lens 22 and a Stimulated Brillouin Scattering (SBS) phase conjugate mirror 23. Preferably, the amplified associated with Oscillator I has tilted edges.

5       The use of a phase-conjugated mirror 23 in the double-pass amplifier design allows the formation of a diffraction-limited beam by compensation of the aberrations in the wavefront which are induced in the first pass by the temperature gradients in the amplifier  
10       rod. In addition, it improves the transverse beam structure allowing the amplifier active element to be pumped more strongly towards its edges without the generation of unwanted diffractive rings. This is because the SBS mirror 23 acts as a beam apodizer,  
15       smoothing the sharp edges of the incoming laser beam owing to lower mirror reflectivity. Greater energy extraction is also possible with a double-pass amplifier scheme without self-excitation. The SBS mirror 23 serves as a selective reflector which reflects only a  
20       coherent signal and not the noise from any amplified spontaneous emission. This is particularly important for efficient amplification of the weaker 1313 nm Nd laser transition.

Amplified radiation from oscillator I (1313 nm) is  
25       then deflected by mirror 24 through half waveplate 25 onto the nonlinear crystal 26 for generation of the second harmonic (here either II-type KTP or BBO, LBO, LiNbO<sub>3</sub> crystal may be used) at 656.5 nm. The beam then travels through half waveplate 27 to another nonlinear  
30       crystal 28 for the generation of the third harmonic (here either I-type LBO or BBO, DKDP or any other suitable crystal may be used) at 437.7 nm. The dielectric mirror 29 is now used to remove the unwanted radiation at 1313 nm.

35       Amplified radiation from oscillator II (at 1053 nm or 1047.1 nm) propagates through half waveplate 25 onto the nonlinear crystal 26 for generation of the second

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harmonic (here either II-type KTP or BBO, LBO, DKDP crystal may be used) at 526.5 nm or 523.6 nm. The dielectric mirror 30 transmits the unwanted radiation at 1053 or 1047.1 nm and combines the radiation at 656.5 nm and 437.7 nm with the radiation at 526.5 nm (or 523.6 nm) thus producing a high energy output beam of multiple colour radiation.

As in preceding section, laser power supplies 4,21 are synchronized through cable 31 to ensure efficient amplification of laser pulses and synchronously or asynchronously emission at 526.5 (523.6) nm, 437.7 nm and 656.5 nm wavelength radiation.

In an alternative embodiment the four Nd:YLF crystals may be replaced by non-birefringent Neodymium-doped Yttrium Aluminium Garnet (Nd:YAG) crystals. The oscillators are otherwise identical to those described above. As before, oscillator I is configured for 1064.2 nm wavelength generation and oscillator II is configured for 1318.8 nm wavelength radiation generation. Because non-birefringent Nd:YAG crystals amplify equally well both orthogonal laser beam polarizations, the two-pass phase conjugated amplifiers may be simplified by replacing the Faraday rotators 18 and 45° polarization rotators 19 with quarter waveplates 32. However, for higher repetition rates (> 5-7 Hz) Nd:YAG amplifiers possess a high depolarization component that could damage the oscillator and which needs to be suppressed by using Faraday isolators.

### An Actively Q-switched Single Frequency Multiple Colour Nd:YLF/Nd:YAG Laser

Fig. 4 shows an Oscillator I of a multiple colour actively Q-switched laser system built around a Neodymium-doped Yttrium Lithium Fluoride (Nd:YLF) crystal. Not shown in Fig. 4 is a second Oscillator II which is identical to the Oscillator I except that the

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optical components are designed and manufactured for use at a different wavelength. Also not shown in Fig. 4 are amplification, harmonic generation and beam combination schemes which are preferably identical to those described above (e.g. elements 16-28 according to the first embodiment and elements 16-32 according to the second embodiment). The actively Q-switched oscillators I,II are configured to generate TEM<sub>00</sub> single frequency radiation for 1313 nm and 1053 nm (or 1047 nm) wavelength generation. Active Q-switching permits higher output energies to be achieved from the oscillator at the same flashlamp pumping energy as in the case of passive Q-switching. Furthermore, active Q-switching ensures low temporal jitter between the electrical synchronization pulse and the laser emission pulse. The typical output energy from the oscillator at 656.5 nm is E = 5-6 mJ, and at 437.7 nm is up to E = 4-5 mJ.

The active Q-switch is formed by a Pockels cell 13 and polarizer 15. High voltage (typically 5-7 kV) is applied to the Pockels cell 13 by an Electro-Optical driver 416 fed by an HV power supply 417 which ensures large initial optical losses in the cavity starting from the flashlamp 2 triggering (signal A) by laser power supply 4. Typically, Pockels cell 13 is made from a LiTaO<sub>3</sub> crystal with three attached gold electrodes. DKDP and LiNbO<sub>3</sub> could alternatively be used, although DKDP has larger absorption losses and LiNbO<sub>3</sub> has a lower damage threshold.

Whilst the flashlamp discharge takes place, the population inversion grows in the Nd:YLF active laser medium. The first spontaneously generated free-running spike is reflected by polarizer 15 to photosensitive diode 418 (e.g. a fast Ge photodiode or InGaAs PIN diode for 1313 nm wavelength radiation; fast Si photodiode for 1053 or 1047.1 nm wavelength radiation) which triggers Prelasing Control driver 419 which is fed by the HV



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power supply 420. As a result, additional voltage (typically 0.5-1 kV) is variably applied to the Pockels cell 13 depending on the intensity of the free-running radiation. Thus a negative feedback loop is formed  
5 thereby providing quasi-CW generation inside the cavity from the moment the first free-running spike appears.

After sufficient quasi-CW generation development time (typically of 20-50  $\mu$ s) the single longitudinal mode is formed inside the laser cavity and propagates. When the  
10 laser power supply 4 produces another Electro-Optical triggering pulse (signal B), the voltage applied by Electro-Optical driver 416 to the Pockels Cell 13 is removed and a Q-switched pulse (of ns duration range) is generated. Delay between flashlamp triggering pulse  
15 (signal A) and Electro-Optical triggering pulse (signal B) is optimized for the highest output energy from the oscillator (typically set of 120-200  $\mu$ s).

An additional stabilization driver 421 can be employed to avoid any sensitivity to the decay of the  
20 flashlamp with time. This ensures long-life stable single longitudinal mode generation. Stabilisation driver 421 measures the delay between the moment the first free-running spike appears and the Electro-Optical triggering pulse (signal B) and keeps this interval  
25 unchanged by driving the voltage of HV Power Supply 417.

In an alternative embodiment, the Nd:YLF crystal in each oscillator I,II may be replaced by a non-birefringent Neodymium-doped Yttrium Aluminium Garnet (Nd:YAG) crystal. However, for stable laser operation  
30 an additional intracavity thin Fabry-Perot etalon 14 (e.g. quartz etalon of 45  $\mu$ m thickness without dielectric coating) is required to suppress competitive generation of 1338 nm.

### 35 Alternative embodiments

In all the embodiments described above the non-linear

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frequency doubling and frequency trebling crystals are placed outside of the ring oscillator. However, alternative embodiments are contemplated wherein in relation to each of the embodiments described above, one  
5 or more of the non-linear crystals could be placed within the ring oscillator cavity.

Since the radiation intensity within the cavity is much larger than outside the cavity, the internal  
10 placement of the frequency conversion crystals leads to a higher harmonic conversion efficiency. Thus for the same pumping energy the RGB output can in principle be higher.

#### Holographic Printing Devices

15 The above embodiments describe RGB laser systems that may, amongst other things, be incorporated into a holographic printer. Holographic printers are devices that print 3-D pictures or holograms onto a special  
20 substrate. Full colour reflection holograms that may be viewed in white light are of particular commercial interest.

Holographic printers can be broadly divided into two categories. The first category pertains to 2-step or  
25 "Master-Write" holographic printers. The second category pertains to 1-step or "Direct-Write" holographic printers. Both categories of printers are discussed in more detail in WO01/45943 (D. Brotherton-Ratcliffe et al.).

#### 30 Direct-Write or 1-Step Holographic Printers

Fig. 5 shows a basic schematic for a 1-step or "Direct-Write" holographic printer. An RGB laser 501  
35 emits visible laser radiation that is split into an object and reference beam by the beam splitter 502. The object beam continues to a beam preparation system 503

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where the beam is expanded, cleaned and otherwise generally prepared in order that it may illuminate the spatial light modulator (SLM) 507 onto which a computer 506 is used to display digitally processed image data.

5 The transmitted radiation passing through SLM 507 is then focused using a special lens system onto a small zone at 510 on the recording material 505. The reference beam co-illuminates this same location 510, having been directed there by a mirror 504. The

10 recording material is moved in a two-dimensional fashion by a servomotor system 509 and a holographic pixel is formed at location 510 each time a laser exposure is made. The specially transformed digital image data is changed at each exposure. In this way a composite

15 hologram that is directly viewable in white light (after processing) may be built up pixel by pixel by directly writing digital data onto the hologram.

#### Master-Write or 2-Step Holographic Printers

20 This type of holographic printer produces an intermediate hologram that must then be transferred or converted into a final white-light viewable hologram. The intermediate hologram is usually referred to as an

25 "H1" hologram or as a "master" hologram. H1 or master holograms are usually transmission holograms but may also be reflection holograms. Without exception they contain images that possess a different optical plane than desired for the final hologram and hence require

30 optical transfer to generate a second hologram possessing the correct optical plane. They may be generated by traditional analogue means or more preferably they may be generated digitally.

An intermediate H1 hologram may most easily be

35 generated digitally by a scheme similar to that shown in Fig. 5, the only difference being that the image data is treated fundamentally differently to image data used in

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1-step holograms. The characteristics of various critical optical elements and the definition of various operational parameters may also be rather different.

In order to produce a final white-light viewable  
5 hologram from a master or H1 hologram, the H1 hologram must be optically transferred as shown, for example, in Fig. 6. Laser radiation is produced by an RGB laser 601 which is then divided, as before, into object and reference beams by the splitter 602. The object beam is  
10 then expanded by the lens 609 before being reflected by the off-axis parabolic mirror 603 onto the processed H1 hologram 604. An unexposed holographic plate 605 is now placed at a distance 608 (the required correction distance for the optical plane) from the H1 and is  
15 illuminated by the first order diffracted radiation produced by the H1. In addition to this object illumination the unexposed holographic plate is illuminated by a reference beam formed by the off-axis parabolic mirror 607, expanding lens 610 and directing  
20 mirror 606. In this way the master or H1 hologram is transferred to a white-light viewable hologram which is also referred to as an "H2" hologram.

Claims

- 5     1. A pulsed multiple colour laser system comprising two or more active laser elements, each said active laser element being provided in a separate laser cavity.
- 10     2. A pulsed multiple colour laser system as claimed in claim 1, wherein second and/or third and/or higher harmonics of laser emissions of said active laser elements are selected and/or generated.
- 15     3. A pulsed multiple colour laser system as claimed in claim 1 or 2, wherein laser emissions at at least a first, second and third wavelength are combined co-linearly to produce a single pulsed laser beam.
- 20     4. A pulsed multiple colour laser system as claimed in claim 3, wherein only said first, second and third wavelengths are combined co-linearly to produce a single RGB pulsed laser beam.
- 25     5. A pulsed multiple colour laser system as claimed in claim 3 or 4, wherein said first wavelength is in the range of 615-680 nm.
- 30     6. A pulsed multiple colour laser system as claimed in claim 5, wherein said first wavelength is selected from the group comprising: (i)  $656.5 \pm 0.5$  nm; (ii)  $669.0 \pm 0.5$  nm; (iii)  $670.7 \pm 0.5$  nm; (iv)  $675.5 \pm 0.5$  nm; and (v)  $659.4 \pm 0.5$  nm.
- 35     7. A pulsed multiple colour laser system as claimed in any of claims 3-6, wherein said second wavelength is in the range of 510-550 nm.

- 20 -

8. A pulsed multiple colour laser system as claimed in claim 7, wherein said second wavelength is selected from the group comprising: (i)  $526.5 \pm 0.5$  nm, (ii)  $523.6 \pm 0.5$  nm; (iii)  $532.1 \pm 0.5$  nm; (iv)  $532.2 \pm 0.5$  nm, (v)  $539.8 \pm 0.5$  nm; and (vii)  $535.0 \pm 0.5$  nm.

9. A pulsed multiple colour laser system as claimed in any of claims 3-8, wherein said third wavelength is in the range of 430-470 nm.

10. A pulsed multiple colour laser system as claimed in claim 9, wherein said third wavelength is selected from the group comprising: (i)  $437.7 \pm 0.5$  nm; (ii)  $446.0 \pm 0.5$  nm; (iii)  $447.1 \pm 0.5$  nm; (iv)  $450.3 \pm 0.5$  nm; and (v)  $439.6 \pm 0.5$  nm.

11. A pulsed multiple colour laser system as claimed in any preceding claim, wherein the laser mode within said laser cavities is arranged to be  $TEM_{00}$  having a single frequency and a single longitudinal mode.

12. A pulsed multiple colour laser system as claimed in any preceding claim, wherein at least one of said active laser elements is arranged in a ring oscillator.

13. A pulsed multiple colour laser system as claimed in claim 12, wherein two active laser elements are provided either: (i) in separate ring oscillators; (ii) in separate linear cavities; or (iii) with one active laser element in a ring oscillator and one active laser element in a linear cavity.

14. A pulsed multiple colour laser system as claimed in any preceding claim, wherein at least one of said active laser elements comprises: (i) Nd:YDF; (ii) Nd:YAP; (iii) Nd:YAG; (iv) Nd:BEL; or (v) Nd in a host matrix other than YDF, YAP, YAG, and BEL.

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15. A pulsed multiple colour laser system as claimed in any preceding claim, wherein at least one said laser cavity is Q-switched.
- 5 16. A pulsed multiple colour laser system as claimed in claim 15, wherein said at least one laser cavity is actively Q-switched.
- 10 17. A pulsed multiple colour laser system as claimed in claim 15, wherein said at least one laser cavity is passively Q-switched.
- 15 18. A pulsed multiple colour laser system as claimed in any preceding claim, further comprising at least one optical amplifier.
- 20 19. A master write holographic laser printer comprising the pulsed multiple colour laser system of any preceding claim.
- 25 20. A master write holographic laser printer as claimed in claim 19 in combination with a hologram preferably a RGB reflection hologram.
21. A hologram produced using the master write holographic laser printer of claim 19.
- 30 22. A single frequency blue pulsed laser system producing laser emission having a wavelength in the range 430-470 nm.
- 35 23. A single frequency blue pulsed laser system as claimed in claim 22, wherein said laser emission is arranged to be TEM<sub>00</sub> having a single longitudinal mode.

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24. A pulsed multiple colour laser system comprising:  
means for generating radiation at a first frequency;  
means for frequency doubling said radiation at said  
first frequency;  
5 means for frequency trebling said radiation at said  
first frequency;  
means for generating radiation at a second frequency;  
and  
means for frequency doubling said radiation at said  
10 second frequency.
25. A pulsed multiple colour laser system as claimed in  
claim 24, further comprising means for combining said  
frequency doubled and frequency trebled radiation so  
15 that either: (i) a co-linear laser beam is provided; or  
(ii) a non co-linear laser beam is provided.
26. A pulsed pan-chromatic or multiple colour laser  
system comprising two oscillators wherein laser  
20 radiation from a first oscillator is frequency doubled  
and trebled and combined with laser radiation from a  
second oscillator which has been frequency doubled.
26. A method of generating laser radiation comprising:  
25 generating laser radiation at a first frequency;  
frequency doubling and frequency trebling said  
radiation at said first frequency;  
generating laser radiation at a second frequency;  
frequency doubling said radiation at said second  
30 frequency; and  
combining said frequency doubled and frequency  
trebled radiation so as to provide a source of pulsed  
pan-chromatic or multiple colour laser radiation.
- 35 27. A digital, analogue or hybrid holographic printer



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comprising a pulsed multiple colour laser.

28. A hologram copying device for producing multiple colour holograms, preferably RGB holograms, comprising a pulsed multiple colour laser system, said copying device either: (i) contact copying for directly producing an identical hologram; and/or (ii) image-plane copying wherein the plane of the image is changed during the copy process.
29. Apparatus for providing a single RGB or multiple colour pulsed laser beam for use in holographic printing.
30. A laser system comprising:  
a first means for generating first pulsed laser radiation;  
a first means for amplifying said first pulsed laser radiation;  
a first means for frequency converting said first pulsed radiation;  
a second means for generating second pulsed laser radiation;  
a second means for amplifying said second pulsed laser radiation; and  
a second means for frequency converting said second pulsed radiation.
31. A laser system as claimed in claim 30, wherein said first and second pulsed laser radiation has a single frequency.
32. A laser system as claimed in claim 30, wherein said first and second pulsed laser radiation has a single longitudinal mode.

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33. A laser system as claimed in claim 31 or 32,  
wherein said first and second pulsed laser radiation is  
formed within a cavity and is arranged to be TEM<sub>00</sub> prior  
to amplification.

5

34.. A pulsed multiple colour laser system comprising:  
two active laser elements each being provided in a  
separate cavity;

an amplifier for amplifying the radiation emitted  
10 from each cavity; and

a frequency conversion device for altering the  
frequency of the radiation.

35. A pulsed multiple colour laser system as claimed in  
15 claim 34, wherein said amplifier further comprises a  
phase conjugate mirror.

36. A pulsed multiple colour laser system as claimed in  
claim 34 or 35, further comprising frequency selective  
20 elements arranged in each cavity so that said radiation  
has a single frequency.

37. A pulsed multiple colour laser system as claimed in  
claim 34, 35 or 36, further comprising spatially  
25 selective elements arranged in each cavity so that said  
radiation has a single spatial mode.

38. A pulsed multiple colour laser system comprising an  
active laser element in a laser cavity, wherein  
30 radiation at a first frequency is frequency doubled and  
trebled to second and third frequencies, wherein said  
frequency doubled radiation has a wavelength in the  
range of 615-680 nm and the frequency trebled radiation  
has a wavelength in the range of 430-470 nm.

35

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39. A pulsed multiple colour laser system as claimed in any of claims 1-18, wherein the time duration of each emitted colour pulse is selected from the group comprising: (i) 1-1000 ps; (ii) 1-1000 ns; (iii) 1-1000  $\mu$ s; (iv) 1-1000 ms; (v) 1-500 ms; (vi) 500-1000 ms; (vii)  $\leq 1$  ms; (viii)  $\leq 500$   $\mu$ s; (ix)  $\leq 200$   $\mu$ s; (x)  $\leq 100$   $\mu$ s; (xi)  $\leq 50$   $\mu$ s; (xii)  $\leq 20$   $\mu$ s; (xiii)  $\leq 10$   $\mu$ s; (xiv)  $\leq 5$   $\mu$ s; (xv)  $\leq 2$   $\mu$ s; (xvi)  $\leq 1$   $\mu$ s; (xvii)  $\leq 500$  ns; (xviii)  $\leq 200$  ns; (xix)  $\leq 100$  ns; (xx)  $\leq 50$  ns; (xxi)  $\leq 20$  ns; (xxii)  $\leq 10$  ns; (xxiii)  $\leq 5$  ns; (xxiv)  $\leq 2$  ns; (xxv)  $\leq 1$  ns.

40. A pulsed multiple colour laser system as claimed in any of claims 1-18 or 39, wherein the amplitude of each emitted colour pulse is selected from the group comprising: (i) 1-1000 nJ; (ii) 1-1000  $\mu$ J; (iii) 1-1000 mJ; (iv) 1-10 J; (v) 1-500 mJ; (vi) 500-1000 mJ; (vii) 1-5 J; and (viii) 5-10 J.

41. A method of generating a pulsed RGB laser beam, comprising the steps of:  
frequency doubling and frequency trebling radiation at a first frequency to provide a red and a blue laser beam, said red laser beam having a wavelength of 615-680 nm and said blue laser beam having a wavelength of 430-470 nm; and  
frequency doubling radiation at a second frequency to provide a green laser beam, said green laser beam having a wavelength of 510-550 nm.

42. The method of claim 41, further comprising the steps of combining said red, blue and green laser beams.

43. A master write holographic printer comprising a pulsed multiple colour laser system.

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44. A master write holographic printer comprising a pulsed multiple colour laser system as claimed in any of claims 1-18.

5 45. A red-blue pulsed laser system comprising an active laser element in a laser cavity, wherein radiation at a first frequency is frequency doubled to provide a red beam having a wavelength in the range of 615-680 nm and frequency trebled to provide a blue beam having a  
10 wavelength in the range of 430-470 nm.

46. A red pulsed laser for generating a red single frequency laser beam having a single longitudinal mode, said laser comprising a Neodymium doped matrix active  
15 laser element arranged in a ring oscillator.

47. A single frequency red pulsed laser system producing laser emission having a wavelength in the range 615-680 nm.  
20

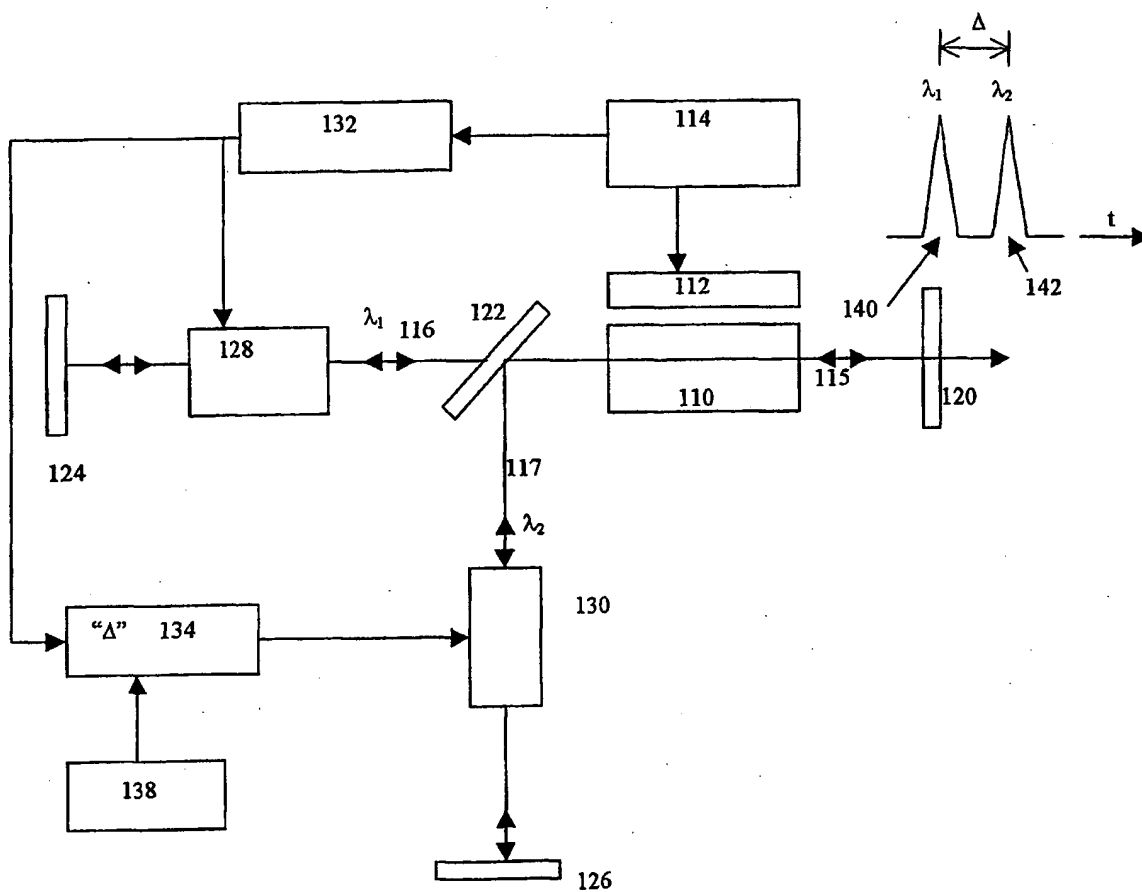
48. A master write holographic printer comprising one, two or three different lasers selected from the following group: (i) a pulsed red laser for generating radiation having a wavelength in the range 615-680 nm;  
25 (ii) a pulsed green laser for generating radiation having a wavelength in the range 510-550 nm; and (iii) a pulsed blue laser for generating radiation having a wavelength in the range 430-470 nm.

30 49. A hologram copying device comprising one, two or three different lasers selected from the following group: (i) a pulsed red laser for generating radiation having a wavelength in the range 615-680 nm; (ii) a pulsed green laser for generating radiation having a  
35 wavelength in the range 510-550 nm; and (iii) a pulsed

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blue laser for generating radiation having a wavelength in the range 430-470 nm.

50. A hologram copying device as claimed in claim 49,
- 5 said copying device either: (i) contact copying for directly producing an identical hologram; and/or (ii) image-plane copying wherein the plane of the image is changed during the copy process.



**FIG.1 - Prior Art**

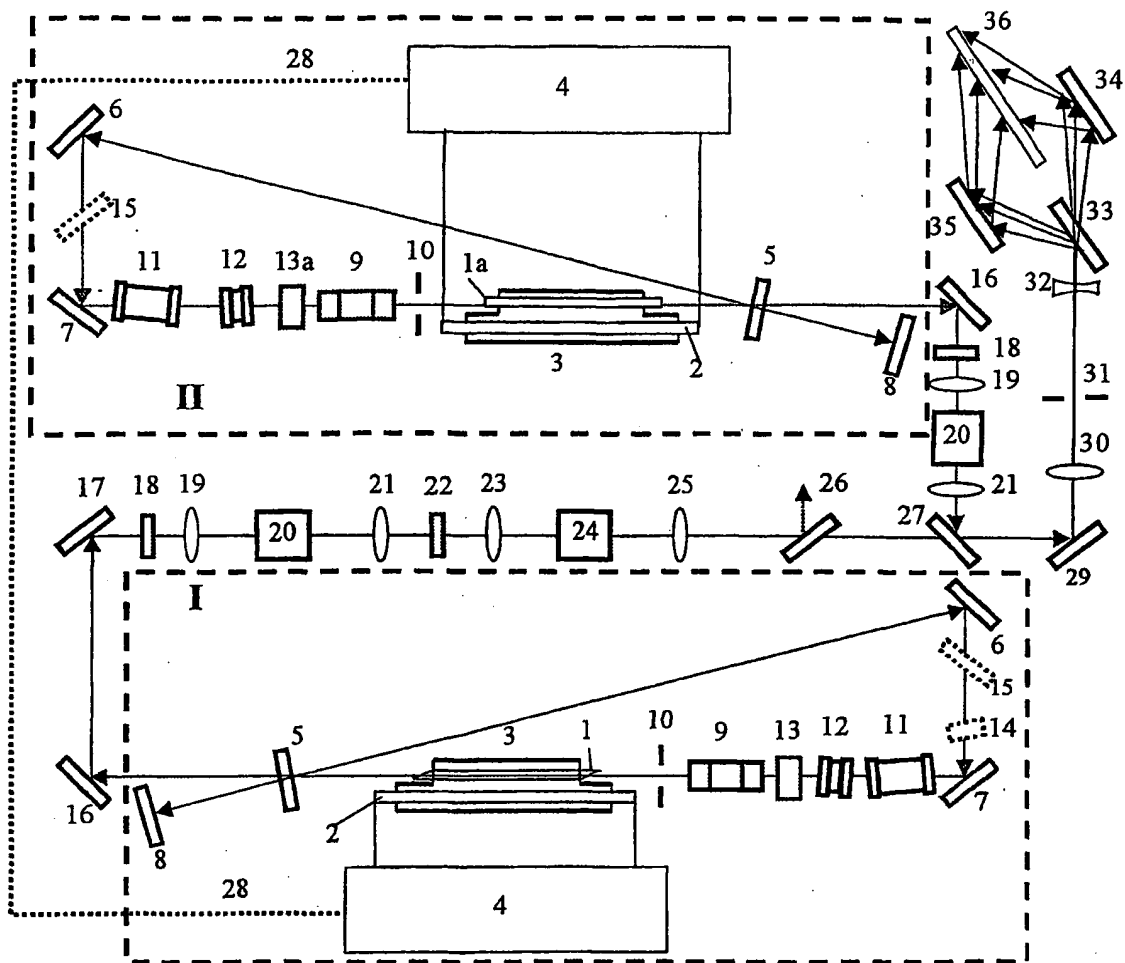


FIG. 2

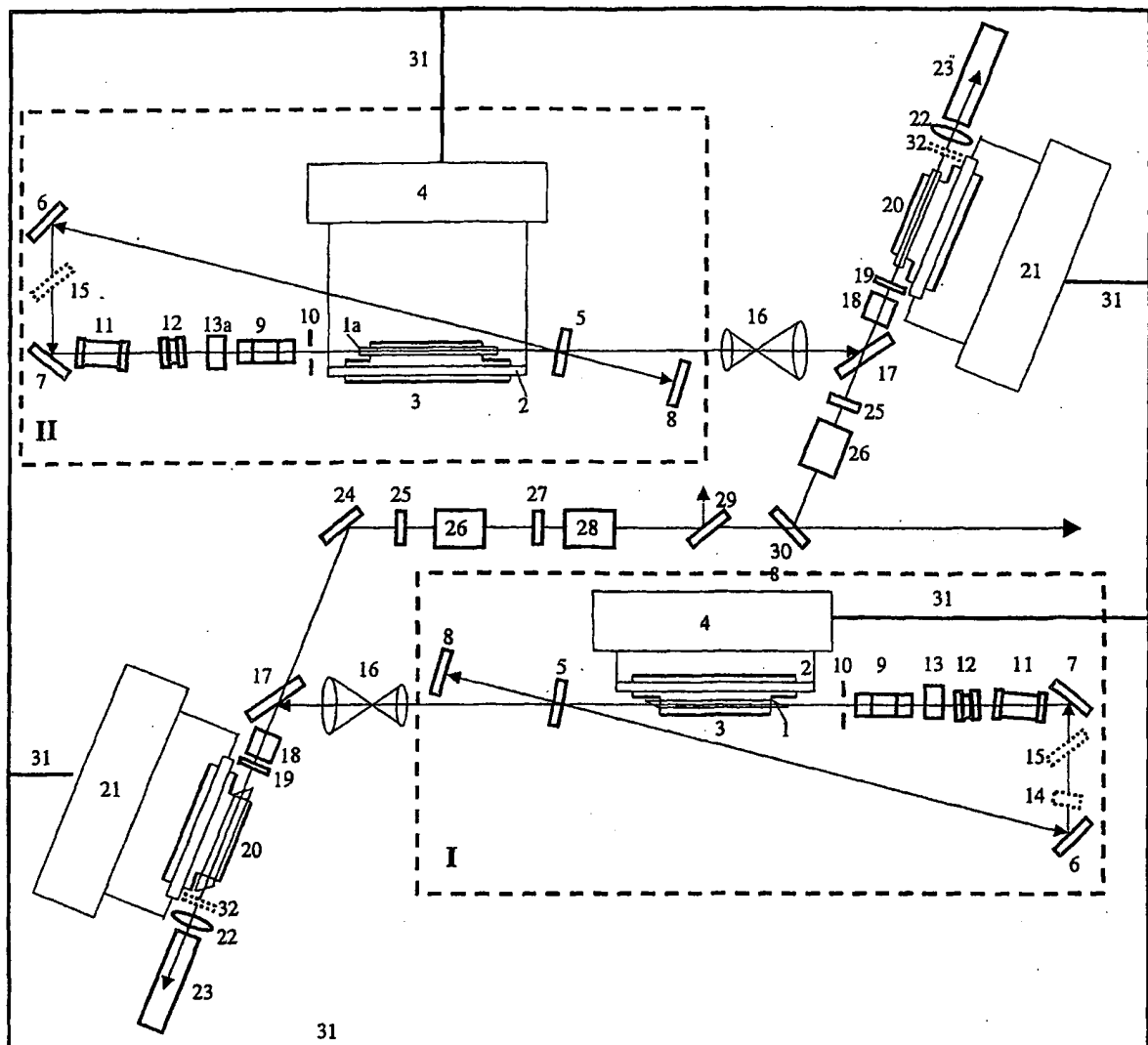


FIG. 3



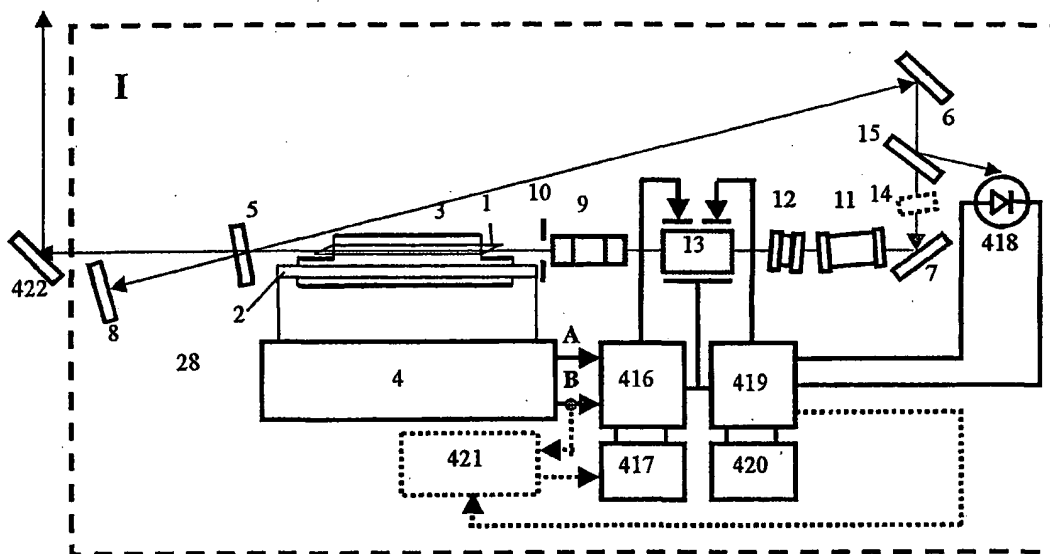
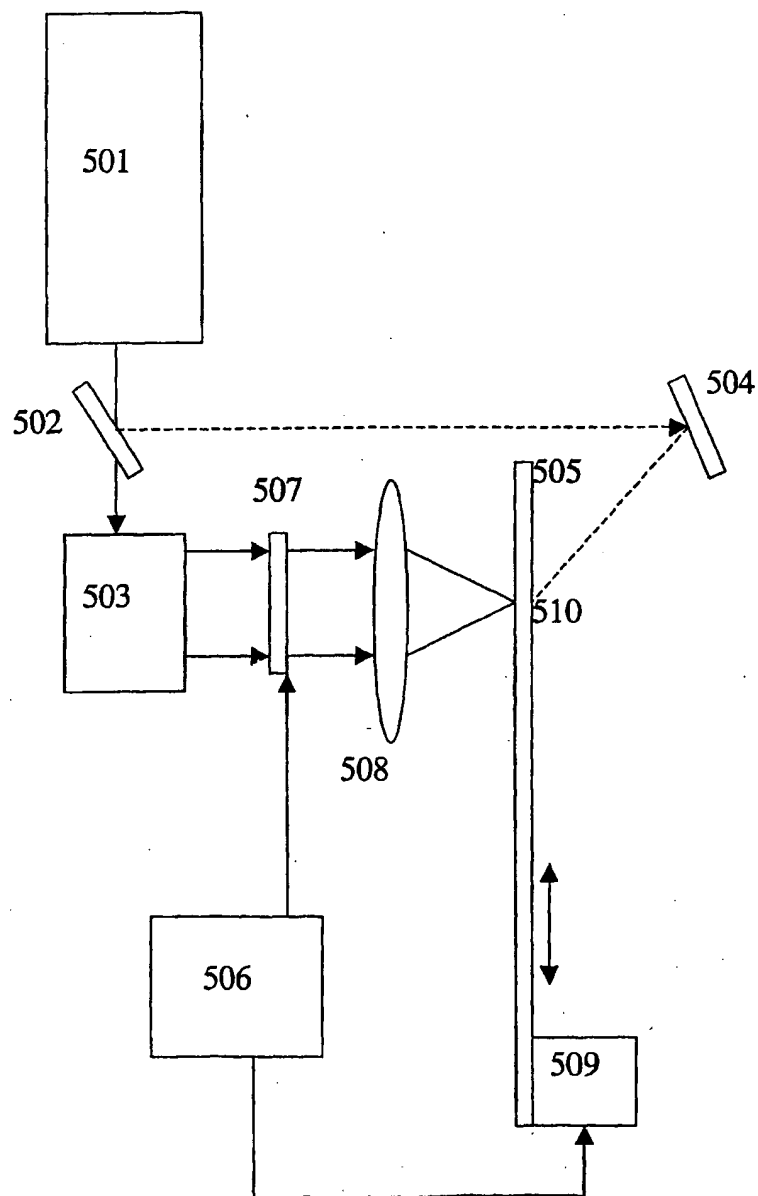
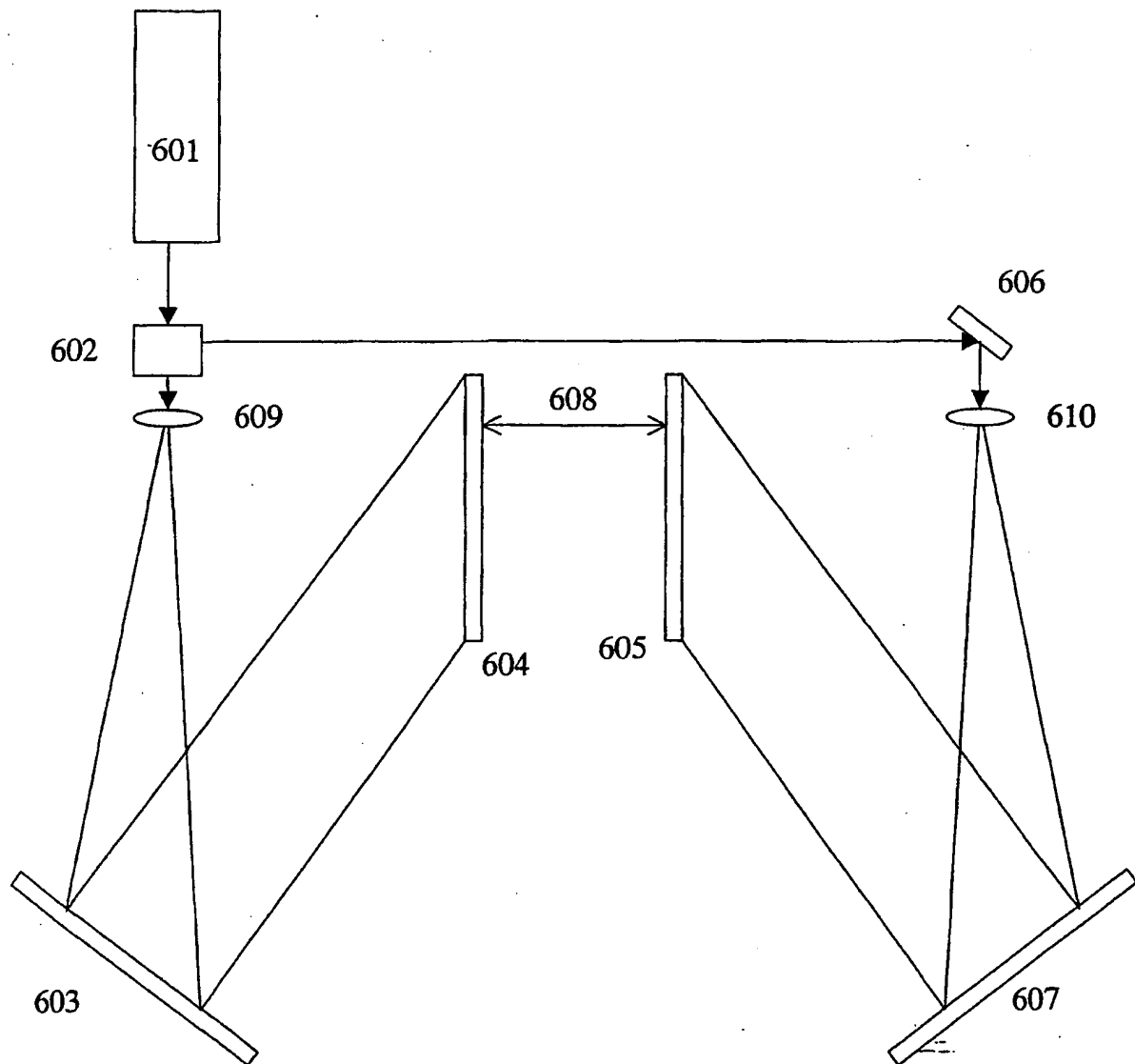


FIG.4

**FIG. 5**

**FIG.6**

## INTERNATIONAL SEARCH REPORT

International Application No  
PCT/GB 01/04460

<b>A. CLASSIFICATION OF SUBJECT MATTER</b> IPC 7 G02F1/35 G03H1/26		
According to International Patent Classification (IPC) or to both national classification and IPC		
<b>B. FIELDS SEARCHED</b> Minimum documentation searched (classification system followed by classification symbols) IPC 7 G02F G03H  Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched  Electronic data base consulted during the International search (name of data base and, where practical, search terms used) WPI Data, PAJ, EPO-Internal, INSPEC		
<b>C. DOCUMENTS CONSIDERED TO BE RELEVANT</b>		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 4 338 578 A (SUKHMAN YEFIM) 6 July 1982 (1982-07-06) column 1, line 7 - line 9 column 1, line 42 -column 2, line 19 column 2, line 33 -column 3, line 34 figure 1	1-4,7,8, 11,14
Y		5,9,12, 13, 15-17, 19-32, 38, 41-45, 47-50
-/--		
<input checked="" type="checkbox"/> Further documents are listed in the continuation of box C. <input checked="" type="checkbox"/> Patent family members are listed in annex.		
<b>* Special categories of cited documents :</b> *A* document defining the general state of the art which is not considered to be of particular relevance *E* earlier document but published on or after the international filing date *L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) *O* document referring to an oral disclosure, use, exhibition or other means *P* document published prior to the international filing date but later than the priority date claimed *T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention *X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone *Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art. *Z* document member of the same patent family		
Date of the actual completion of the international search  11 January 2002		Date of mailing of the international search report  18/01/2002
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016		Authorized officer  Krametz, E

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International Application No  
PCT/GB 01/04460

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
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International Application No

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